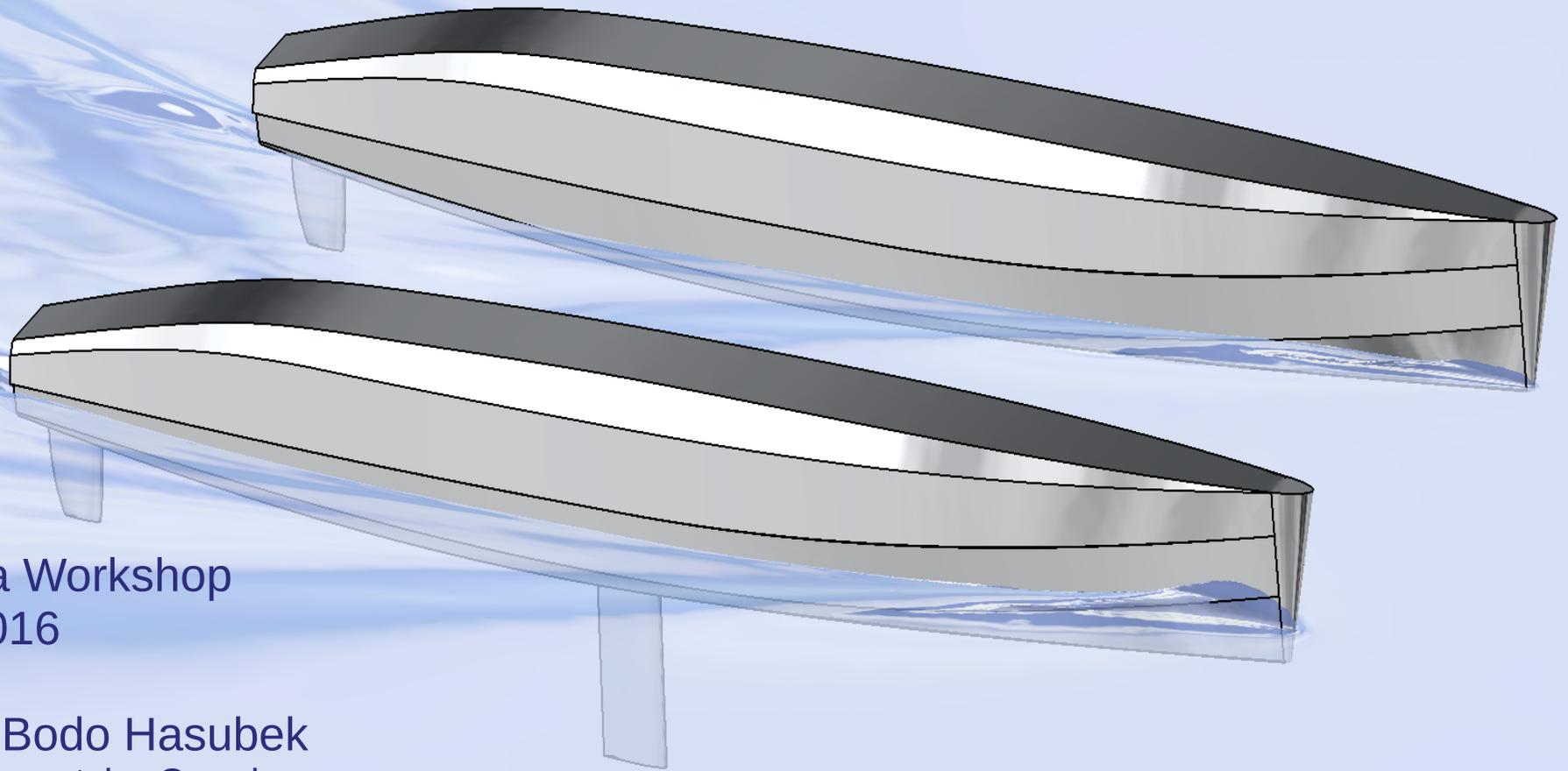


# Virtual tank testing for a VPP of a sailing catamaran



Numeca Workshop  
SMM 2016

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# The Project: Dreamcatcher One

A cruising catamaran for worldwide travel

## Key properties

- Length 20.57m
- Max. width 10.67m
- BCB 4.25m
- Mast height 30.0m
- Sail area 270m<sup>2</sup>
- Weight 36.0t
- Material Aluminium
- Other Daggerboards



# Motivation

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Why going through the effort of using a CFD in a yacht design?

- More realistic force calculations for optimized hull geometries
- Catamaran designs
  - Interaction between hulls can be captured (in leeway conditions as well)
  - Lift/Sinkage of hulls in heeled conditions
  - Very limited catamaran designs in Delft series
- Appendages and their interaction can be properly described



More realistic performance estimate

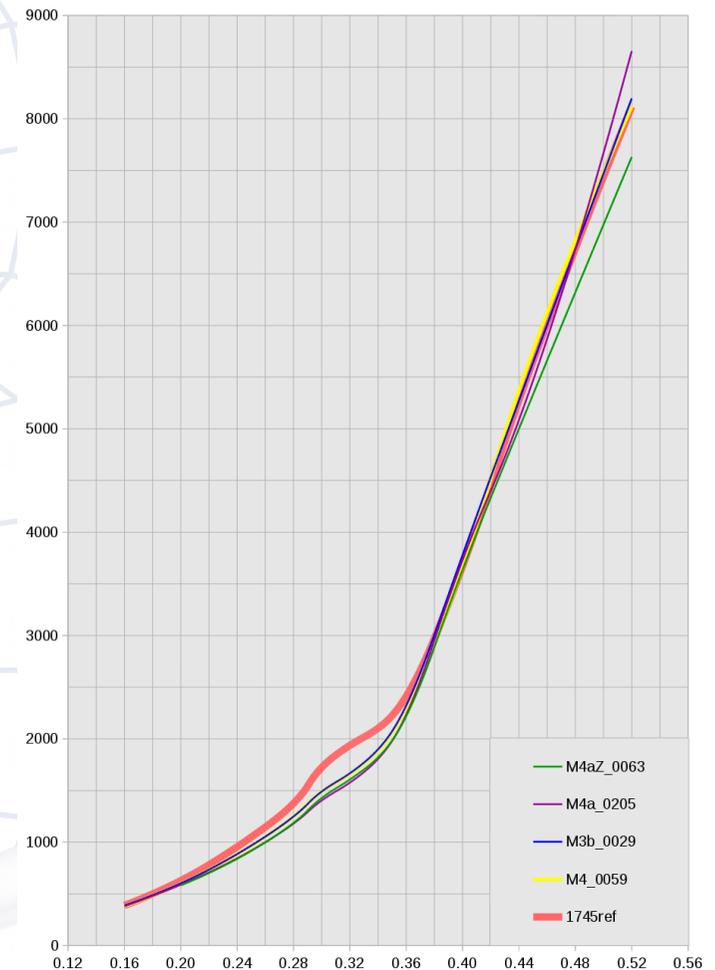
# Systematic Hull Variation

Optimization goal:

Best performance at 8-10 kts ( $F_n=0.3\dots0.36$ )

Setup using CAESES

- **Unappended, single hull**
- 4508 models in total
- 3987 wave resistance analysed (potential flow)
- 521 combined potential flow and Navier-Stokes (VOF) analysis
- Reduced total resistance at 8kts by 15% compared to best analytical design using “good” design criteria



# Model for Fine/Marine

## Appended hull

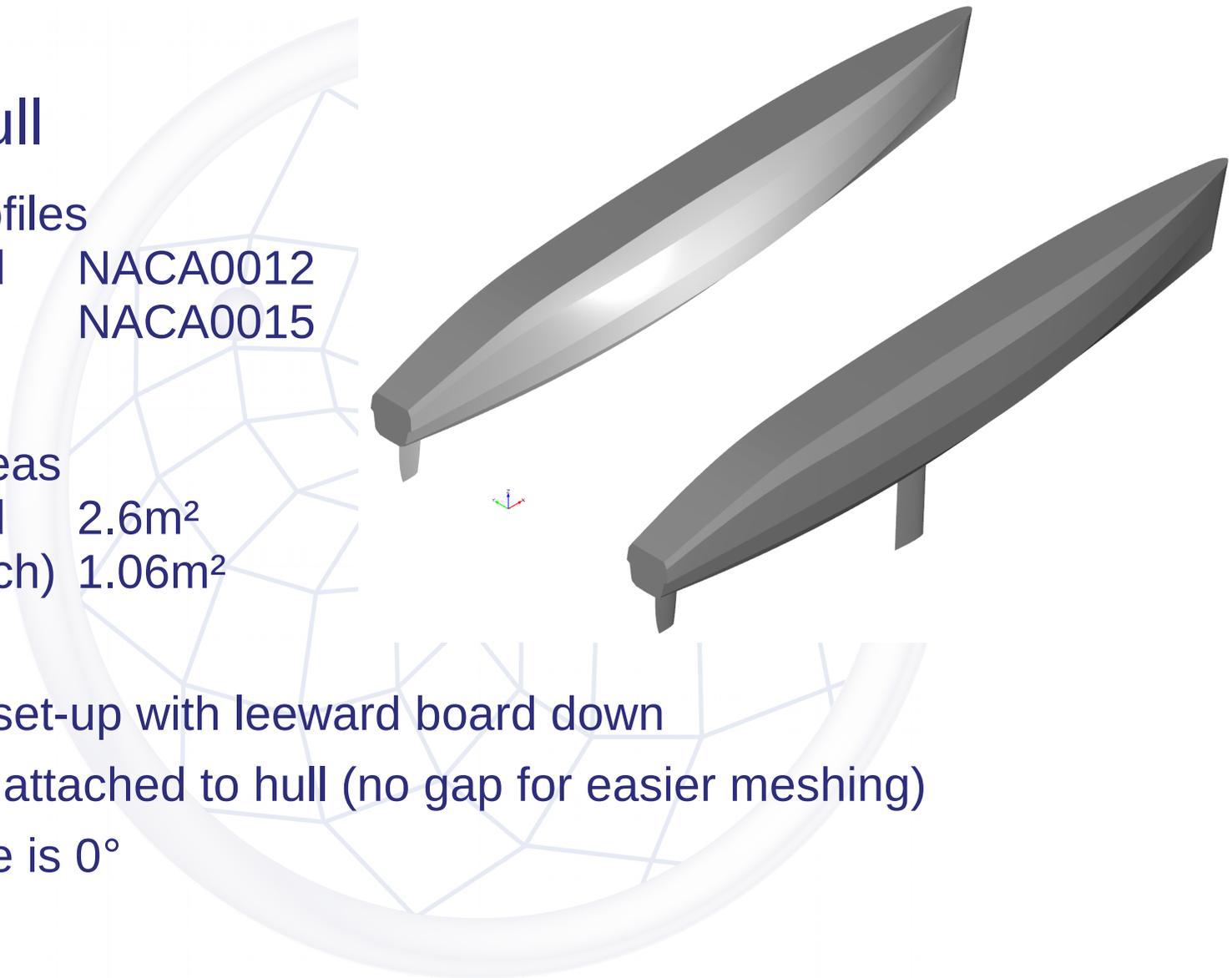
- Standard profiles

Daggerboard	NACA0012
Rudders	NACA0015

- Projected areas

Daggerboard	2.6m <sup>2</sup>
Rudders (each)	1.06m <sup>2</sup>

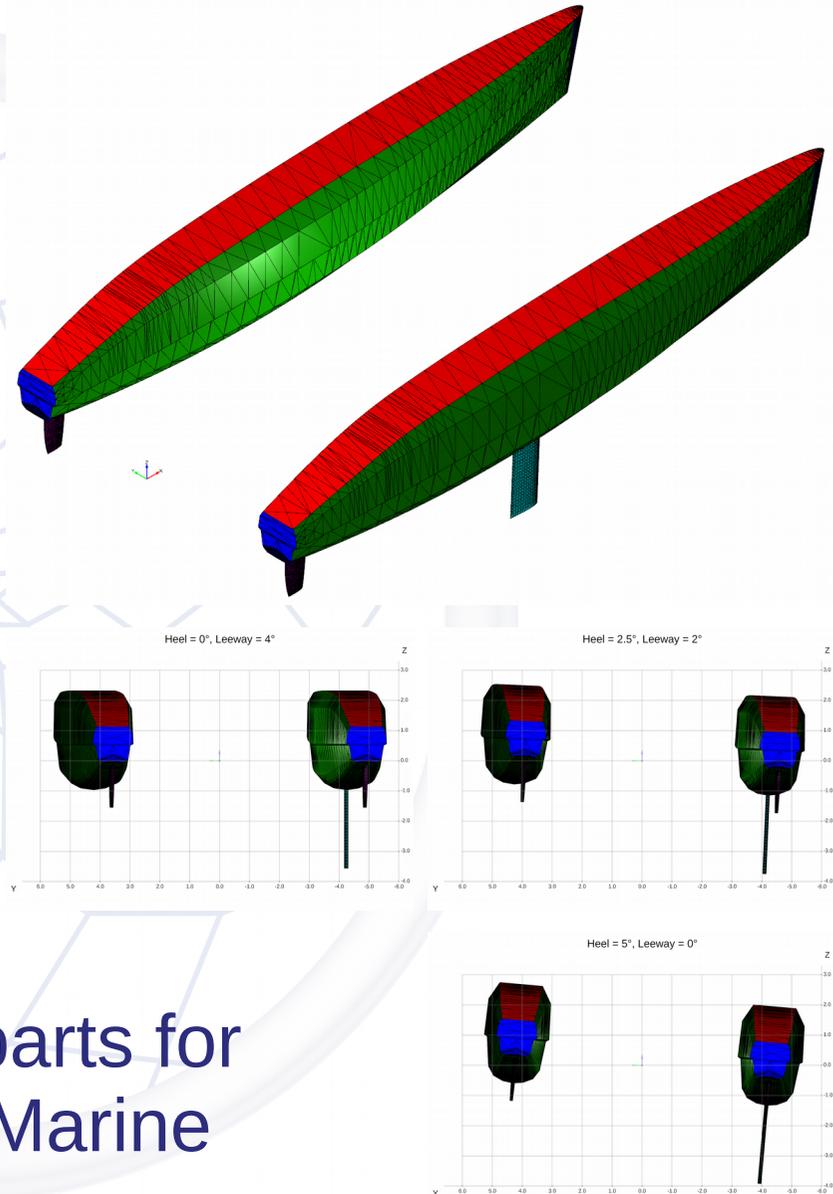
- Asymmetric set-up with leeward board down
- Rudders are attached to hull (no gap for easier meshing)
- Rudder angle is 0°



# Model setup for Fine/Marine

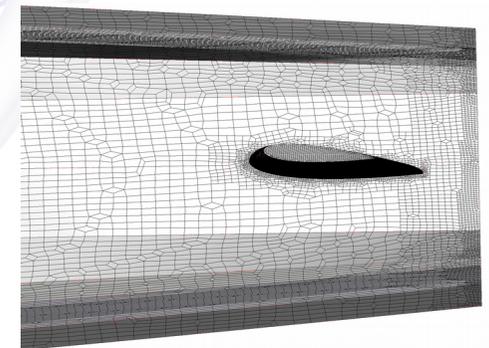
## Model setup workflow

- Parametric model in CAESES
  - Heel / Leeway transformations
  - Fixed displacement
  - Variable rudder angles and daggerboard sweep angles
- Triangulation in CAESES
  - Water-tight STL body
  - STL-triangulation exported (multibody STL)
- Different colours for different parts for automatic recognition in Fine/Marine



# Meshing in Fine/Marine

- Fine/Marine Wizard for base set-up
- Manual Mesh refinement of bow and daggerboard and rudders to properly capture sharp discontinuities in curvature
- Between 5 and 7 mio. cells (Larger number for larger heel/leeway angles)
- Grid quality measures were ruined by edge above the waterline
- Grid sensitivity analysis showed little influence on results for increased number of cells



# Virtual tank tests

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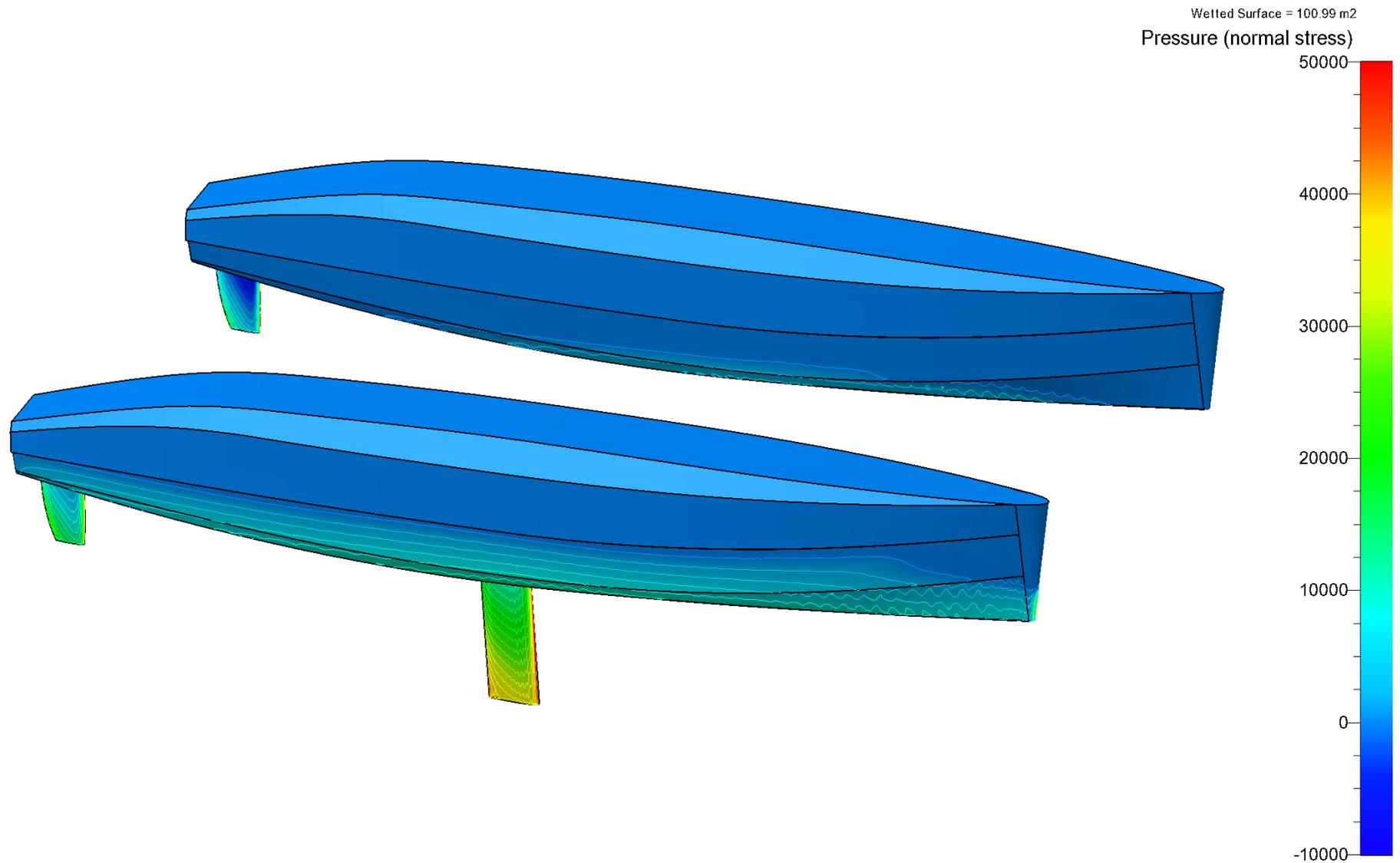
- Test range

- Velocities 4-14kts ( $F_n=0.15-0.52$ )
- Heel  $0.0^\circ - 5.0^\circ$
- Leeway  $0.0^\circ - 4.0^\circ$
- Total 4 velocities each  
16 models at different angle combinations  
64 calculations

- Calculation effort

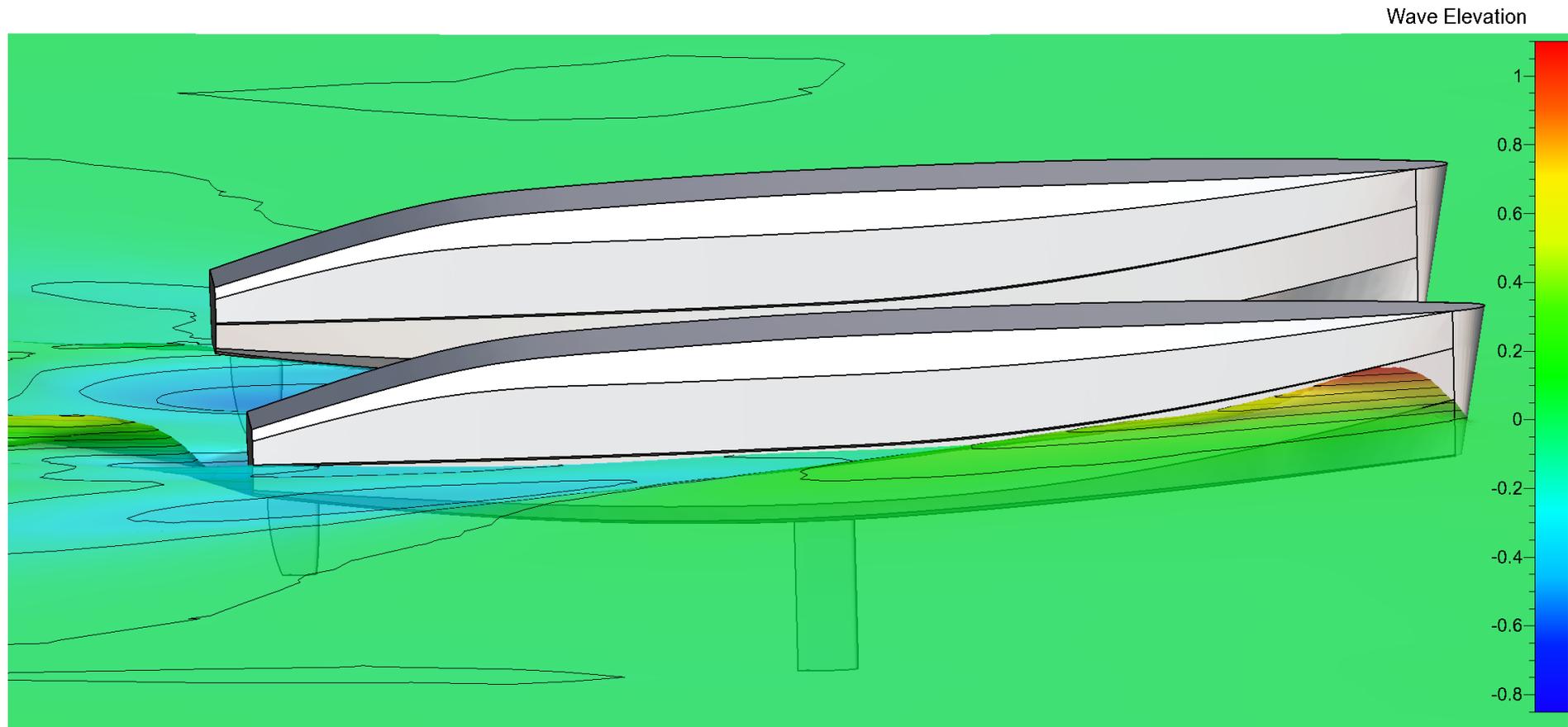
- Hardware 8-core Haswell running at 3.0/3.5 GHz  
64 GB RAM (no swapping)
- Average calc. time 29.1 hours (per calculation)
- Total calc. time 77 days

# Results: Visual inspection 1



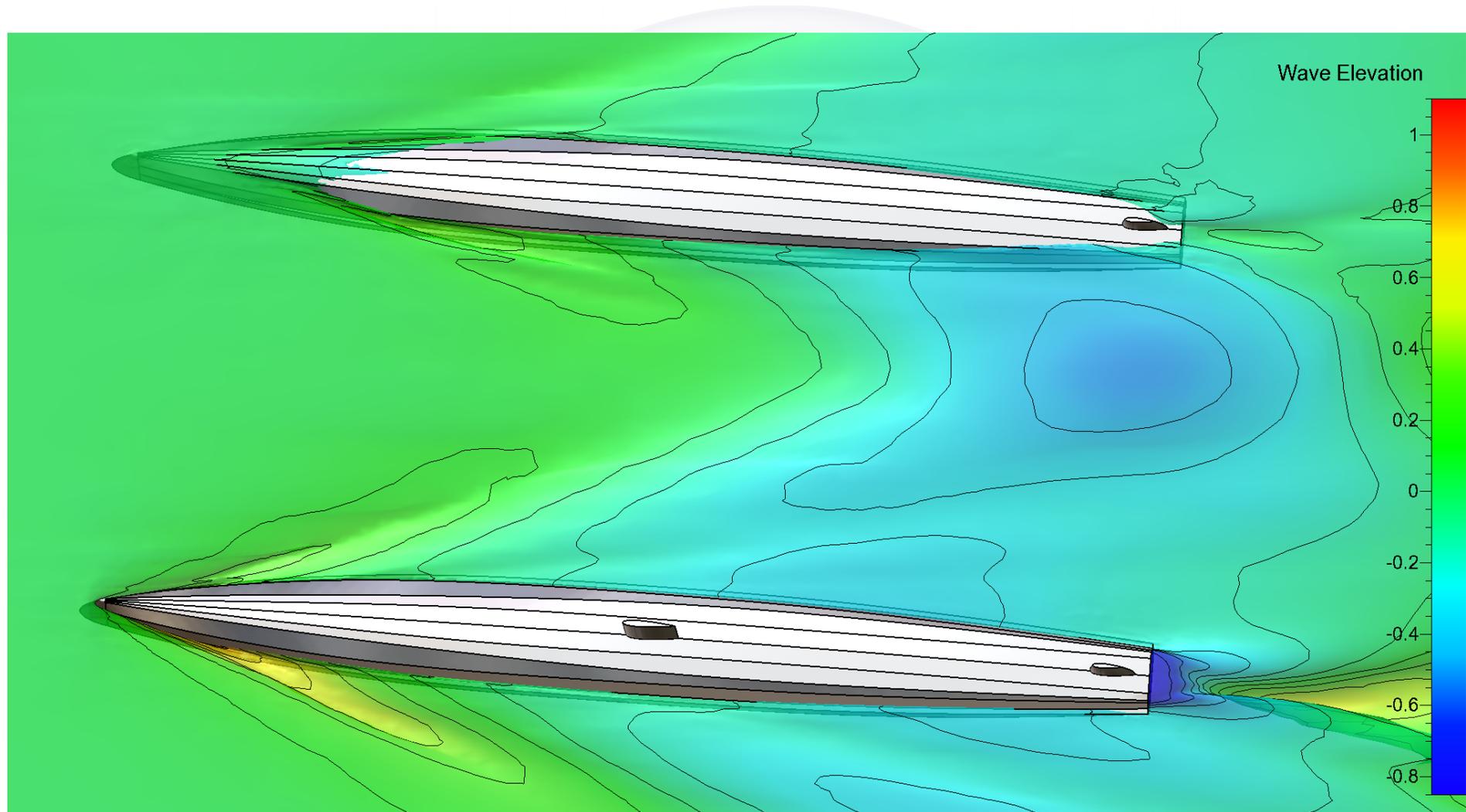
Pressure distribution: rectangular shape vs. elliptical appendage shapes

# Results: Visual inspection 2



Wave elevation: Clean run-off at the submerged hull

# Results: Visual inspection 3



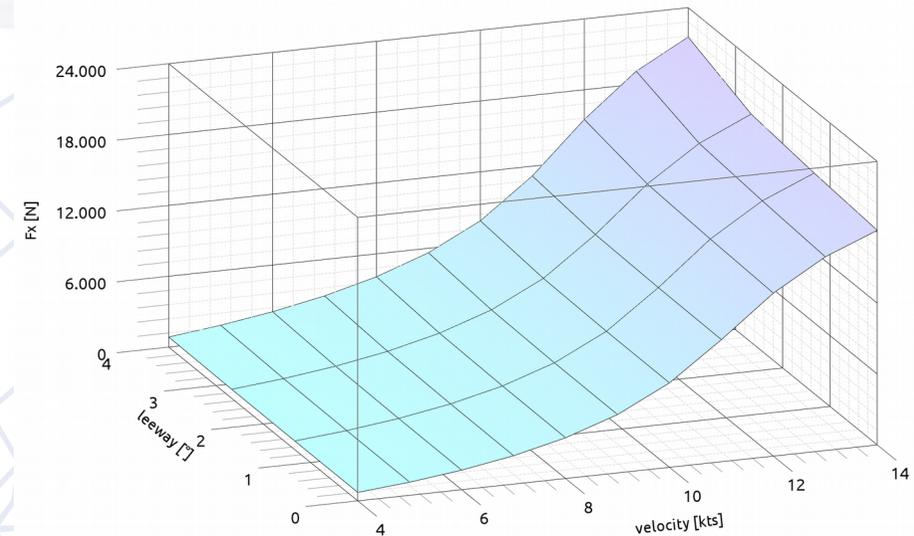
Wave elevation: Bottom view, no rudder ventilation

# Results: Resistance and side forces

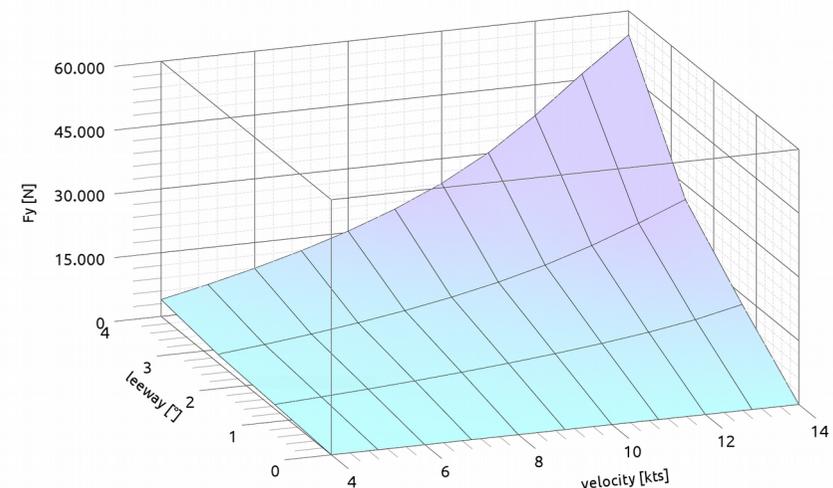
## Numerical results

- Resistance forces in global x direction
  - Confirms results from systematic hull variation series:  
No bump at  $Fn = 0.3$  (8kts)
  - Influence of leeway
  - One such surface for each heel angle
- Side forces perpendicular to mid-ship line
  - Highly efficient appendages
  - Side forces of one daggerboard sufficient to balance sail side forces

Resistance at 2.5° heel



Side Force at 2.5° heel



# Velocity Prediction Program (VPP)

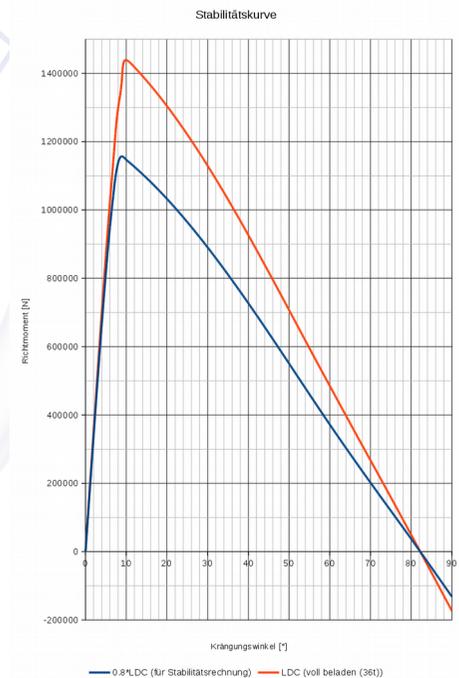
## Balancing of hull and sail forces

- ORC only uses two (equations (1) and (3))
- Here  $F_y$ -equilibrium (2) is used in addition to determine leeway angle
- CFD calculations deliver  $F_x$  and  $F_y$ , static stability curve delivers  $M_x$  of the hull
- Sailmodel delivers  $F_x$  and  $F_y$  of the sails, and the heeling arm to determine  $M_x$
- Balancing is done using the Newton-Raphson-Method

$$F_x^A = F_x^H \quad (1)$$

$$F_y^A = F_y^H \quad (2)$$

$$M_x^A = M_x^H \quad (3)$$



# Hull resistance and side force model

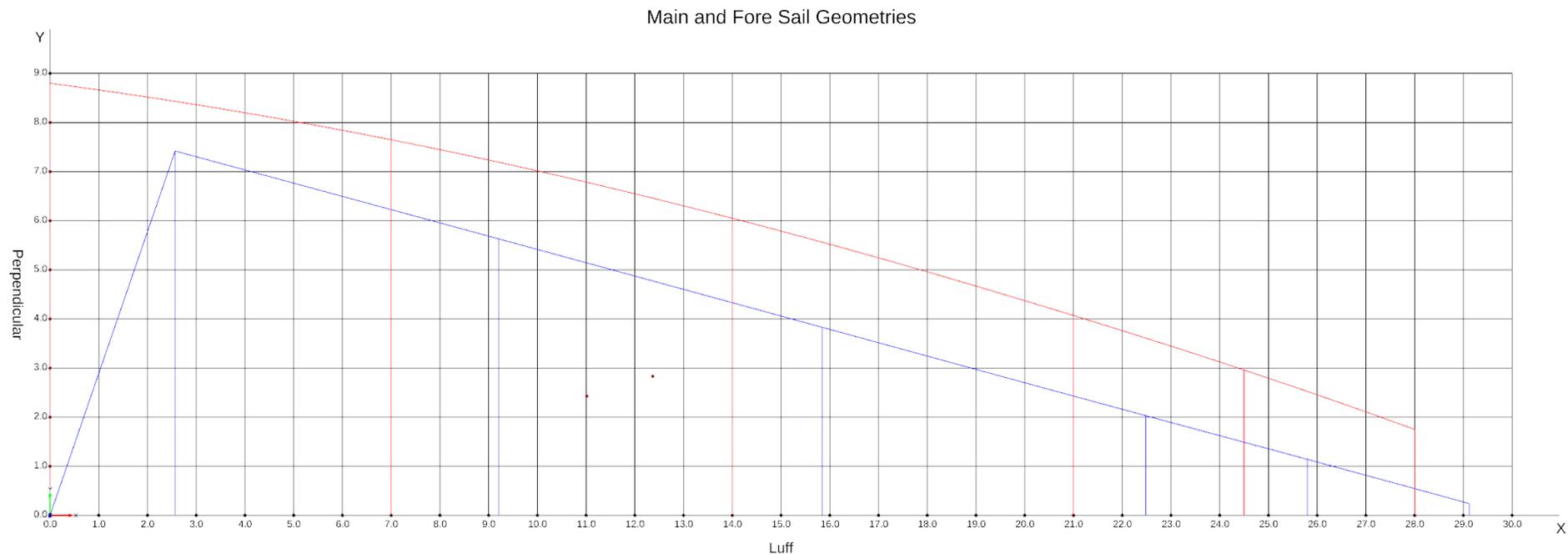
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3-dimensional B-spline interpolation for scattered data using the simulation data for  $F_x$  and  $F_y$

- Uses 4<sup>th</sup> order B-splines
- Proper non-linear interpolation
- Grid refinement procedure allows for close approximation of calculated data
- Differentiable (important for Newton-Raphson)
- Can be extrapolated

# Sail Model

- Uses an adapted ORC model
  - Sail areas and centre of effort are derived from exact geometric representation of the sails including reefing (ORC uses simple trapezoidal rule)
  - Lift and Drag coefficients are taken from the ORC



# Advantages/Disadvantages

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## Advantages

- Arbitrary hull shapes
  - Multihulls
  - Hard chines
- Independent of systematic series
- Unusual appendage configurations
- Bonus: Moments around vertical axis for boat balance considerations

## Disadvantages

- Only flat water simulation (no waves)
- Calculation effort

# Thank you

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**Questions?**

More information on my project:  
[www.dreamcatcherone.de](http://www.dreamcatcherone.de) (German only)